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# Spectral Analysis and scaling relations of Cairo Earthquake sequence of Oct. 12,1992 recorded at KEG VBB Station 

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#### Abstract

Spectral analysis of fifty six KEG VBB records from Cairo earthquake source region is preformed to obtain the source parameters such as the seismic moment, source radius and stress drop. These parameters are used in turn to obtain empirical local magnitude (ML)- Seismic moment (Mo) - Coda duration (D) relations for that region. In this study the data consist of $\mathbf{L g}$ waves on the vertical component seismograms for earthquakes of ML between $\mathbf{1 . 7}$ and 4.7. The mainshock has a seismic moment (Mo) of $\mathbf{1 . 3 7 \times 1 0 ^ { 2 4 }}$ dyne.cm, a source radius of $\mathbf{1 . 3} \mathbf{~ k m}$ and stress drop of $\mathbf{2 7 0}$ bar. For the aftershock sequence, the derived empirical relation between the seismic moment (Mo) and ML for magnitude range $1.7<\mathbf{M L}<4.7$ is


$$
\log (\mathrm{Mo})=(0.96 \pm 0.2) M L+(17.89 \pm 0.56)
$$

Stress drops of the events under study lies in the range between ( $0.12-120 \mathrm{bar}$ ). It tends to increase with increasing seismic moment in the range less than $10^{21}$ dyne.cm but appear to be constant at greater values. The estimated source radius in nearly constant.
Radiated energy released (Es) were calculated for these aftershocks from the shear wave velocity time series. The radiated energy is related with seismic moment and local magnitude by:

$$
\begin{gathered}
\log (E s)=(1.752 \pm 0.03) \mathrm{ML}+(12.86 \pm 0.09) \\
\log (\mathrm{Es})=(1.74 \pm 0.059) \log (\mathrm{Mo})-(18.07 \pm 1.2)
\end{gathered}
$$

## 1-Introduction

On the $12^{\text {th }}$ of October 1992 a moderate Size earthquake of $\mathbf{M}_{\mathbf{w}}=\mathbf{5 . 8}$ occurred at epicentral distance of about $\mathbf{2 5 ~ K m}$ south west of the Cairo city in Dahshour region at a depth of 22 km (Fig1). This earthquake was felt from Alexandria to Aswan. It registered a maximum observed intensity of 7 in MSK intensity scale in Dahshour region. This shock caused considerable damage to the buildings in four districts: Eastern part of Cairo, Giza and its suburb and Northern area of Fayoum. Significant damage was found mostly in adobe or old non-reinforced brick masonry buildings and non-engineering reinforced concrete building. In addition extensive liquefaction of deltaic silty sand deposits was observed in some villages of Giza City located $\mathbf{1 9} \mathbf{~ k m}$ from the epicenter. According to eyewitness sand and water continuously below up to a height of $\mathbf{3} \mathbf{~ m}$ for about $\mathbf{4 5}$ minutes.

The Cairo earthquake has struck in a previously low seismicity area. The only significant earthquake reported in this region during the historical period occurred in 1847. The mainshock was followed by aftershocks activity. Within twenty two days after the occurrence of Cairo earthquake 55 shocks with $\mathbf{1 . 7}<\mathbf{M L}<\mathbf{4} .7$ were recorded by KEG Broad Band station. Event data are given in table 1. Fig (2) shows the distribution of the well located aftershocks of the Cairo earthquake sequence of 1992 recorded by a temporary seismic network installed by National Research Institute of Astronomy and Geophysics during the first twenty days of this sequence. Details about the seismic network and procedure of determination the hypocenters are given by Abou El enein,et al. 1999. The pattern of the aftershocks reflects a cluster rather than a clear trend of seismicity.


Figure (1): Dahshour area and its location related to Cairo city.


Fig (2): Dahshour aftershocks distributions.

Table (1): Hypocentral locations of the events under study as the result of the Hypo71 software.

| \# | $\begin{gathered} \text { Date } \\ \text { Y M D } \end{gathered}$ | $\begin{aligned} & \text { Origin Time } \\ & \mathrm{H} \mathrm{~m} \mathrm{~s} \\ & \hline \end{aligned}$ | Lat ${ }^{\circ} \mathrm{N}$ | $\operatorname{Lon}^{\circ} \mathrm{E}$ | Depth(Km) | $\begin{gathered} \hline \text { MD } \\ \text { (HLW) } \end{gathered}$ | ML |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $\begin{gathered} 92101 \\ 2 \end{gathered}$ | 13955.87 | 29-50.83 | 31-2.29 | 23.20 | 5.3 | 5.96 |
| 2 | $\begin{gathered} 92101 \\ 2 \end{gathered}$ | 13509.65 | 29-46.94 | 31-13.66 | 10.93 |  | 2.52 |
| 3 | $\begin{gathered} 92101 \\ 2 \end{gathered}$ | 14118.64 | 29-43.33 | 31-9.12 | 18.84 |  | 2.31 |
| 4 | $\begin{gathered} 92101 \\ 2 \\ \hline \end{gathered}$ | 14157.43 | 29-57.23 | 30-57.28 | 25.09 |  | 2.81 |
| 5 | $\begin{gathered} 92101 \\ 2 \end{gathered}$ | 145814.73 | 29-52.55 | 31-14.55 | 22.32 |  | 1.84 |
| 6 | $\begin{gathered} 92101 \\ 2 \\ \hline \end{gathered}$ | 150742.05 | 29-53.52 | 31-6.80 | 26.85 |  | 2.34 |
| 7 | $\begin{gathered} 92101 \\ 2 \\ \hline \end{gathered}$ | 152524.65 | 29-52.48 | 31-6.83 | 29.55 |  | 4.7 |
| 8 | $\begin{gathered} 92101 \\ 2 \end{gathered}$ | 155250.77 | 29-51.24 | 31-9.94 | 22.77 |  | 2.26 |
| 9 | $\begin{gathered} 92101 \\ 2 \\ \hline \end{gathered}$ | 16559.79 | 29-50.29 | 31-11.01 | 25.59 |  | 2.37 |
| 10 | $\begin{gathered} 92101 \\ 2 \end{gathered}$ | 183142.36 | 29-47.89 | 31-9.82 | 21.14 |  | 2.24 |
| 11 | $\begin{gathered} 92101 \\ 2 \\ \hline \end{gathered}$ | 195559.20 | 29-51.15 | 31-13.38 | 19.10 |  | 2.19 |
| 12 | $\begin{gathered} 92101 \\ 2 \end{gathered}$ | 213134.22 | 29-40.00 | 31-7.06 | 20.73 |  | 4.15 |
| 13 | $\begin{gathered} 92101 \\ 2 \\ \hline \end{gathered}$ | 214616.02 | 29-43.61 | 31-13.10 | 9.83 | 2.9 | 2.45 |
| 14 | $\begin{gathered} 92101 \\ 2 \\ \hline \end{gathered}$ | 233422.50 | 29-55.72 | 31-16.90 | 17.10 | 3.0 | 2.69 |
| 15 | $\begin{gathered} 92101 \\ \hline \end{gathered}$ | 234624.42 | 29-44.40 | 31-10.38 | 21.78 | 2.9 | 2.13 |
| 16 | $\begin{gathered} 92101 \\ \hline 3 \end{gathered}$ | 18098.14 | 29-52.44 | 31-10.98 | 22.39 | 3.4 | 3.67 |
| 17 | $\begin{gathered} 92101 \\ 3 \\ \hline \end{gathered}$ | 183454.26 | 29-50.62 | 31-13.15 | 20.72 |  | 3.16 |
| 18 | $\begin{gathered} 92101 \\ 3 \\ \hline \end{gathered}$ | 232756.39 | 29-53.00 | 31-7.37 | 32.02 | 2.4 | 2.22 |
| 19 | $\begin{gathered} 92101 \\ 4 \end{gathered}$ | 024423.14 | 29-52.16 | 31-9.69 | 30.25 | 3.1 | 2.77 |
| 20 | $\begin{gathered} 92101 \\ 4 \\ \hline \end{gathered}$ | 035014.53 | 29-46.63 | 31-6.43 | 29.49 | 3.4 | 2.76 |
| 21 | $\begin{gathered} 92101 \\ 4 \\ \hline \end{gathered}$ | 094027.04 | 29-43.49 | 31-1.28 | 27.64 | 4.0 | 4.17 |
| 22 | $\begin{gathered} 92101 \\ 4 \\ \hline \end{gathered}$ | 104157.34 | 29-46.67 | 31-7.99 | 22.95 | 2.6 | 1.94 |
| 23 | $\begin{gathered} 92101 \\ \hline 4 \end{gathered}$ | 120915.72 | 29-43.34 | 31-5.99 | 20.53 |  | 2.95 |
| 24 | $\begin{gathered} 92101 \\ 4 \\ \hline \end{gathered}$ | 134639.47 | 29-50.45 | 31-10.37 | 28.51 | 3.5 | 3.22 |
| 25 | $\begin{gathered} 92101 \\ 4 \end{gathered}$ | 142344.67 | 29-41.18 | 31-14.42 | 20.22 | 3.1 | 2.4 |


| \# | $\begin{gathered} \hline \text { Date } \\ \text { YM D } \end{gathered}$ | Origin Time H m s | Lat ${ }^{\circ} \mathrm{N}$ | Lon ${ }^{\circ} \mathrm{E}$ | Depth(Km) | $\begin{gathered} \hline \text { MD } \\ \text { (HLW) } \end{gathered}$ | ML |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 | $\begin{gathered} 92101 \\ 4 \end{gathered}$ | 143127.90 | 29-43.41 | 31-6.98 | 24.97 | 3.3 | 2.92 |
| 27 | $\begin{gathered} 92101 \\ 4 \\ \hline \end{gathered}$ | 201611.05 | 29-49.25 | 31-9.74 | 20.94 | 2.6 | 2.29 |
| 28 | $\begin{gathered} 92101 \\ 5 \end{gathered}$ | 121341.41 | 29-48.25 | 31-9.02 | 25.52 | 2.6 | 1.96 |
| 29 | $\begin{array}{\|c} 92101 \\ 6 \\ \hline \end{array}$ | 032851.46 | 29-47.29 | 31-5.79 | 24.12 | 2.5 | 1.99 |
| 30 | $\begin{gathered} 92101 \\ 6 \end{gathered}$ | 055611.84 | 29-47.31 | 31-3.17 | 30.70 | 3.1 | 2.91 |
| 31 | $\begin{array}{\|c} \hline 92101 \\ 6 \\ \hline \end{array}$ | 095746.87 | 29-47.50 | 31-5.51 | 26.25 | 3.3 | 3.08 |
| 32 | $\begin{array}{\|c} \hline 92101 \\ 6 \\ \hline \end{array}$ | 180753.12 | 29-51.50 | 31-7.49 | 24.20 | 2.6 | 2.4 |
| 33 | $\begin{gathered} 92101 \\ \hline 7 \\ \hline \end{gathered}$ | 013528.51 | 29-45.06 | 31-8.25 | 25.44 | 2.6 | 2.03 |
| 34 | $\begin{gathered} 92101 \\ 8 \end{gathered}$ | 081216.12 | 29-43.38 | 31-8.40 | 20.74 | 3.4 | 2.86 |
| 35 | $\begin{gathered} 92101 \\ 8 \end{gathered}$ | 130428.44 | 29-42.75 | 31-13.80 | 18.50 | 3.0 | 2.61 |
| 36 | $\begin{gathered} 92101 \\ 9 \\ \hline \end{gathered}$ | 104630.95 | 29-42.67 | 31-9.58 | 21.58 | 2.9 | 2.23 |
| 37 | $\begin{gathered} 92101 \\ 9 \end{gathered}$ | 123016.44 | 29-44.22 | 31-6.30 | 25.20 | 3.2 | 2.99 |
| 38 | $\begin{gathered} 92101 \\ 9 \end{gathered}$ | 145950.43 | 29-44.50 | 31-8.87 | 18.68 | 3.3 | 3.17 |
| 39 | $\begin{gathered} 92102 \\ 0 \end{gathered}$ | 060030.77 | 29-32.36 | 31-4.27 | 22.28 | 2.7 | 1.65 |
| 40 | $\begin{gathered} 92102 \\ 0 \\ \hline \end{gathered}$ | 172828.44 | 29-40.39 | 31-9.24 | 20.62 | 2.5 | 1.98 |
| 41 | $\begin{gathered} 92102 \\ 0 \\ \hline \end{gathered}$ | 231447.46 | 29-43.08 | 31-7.65 | 17.20 | 3.1 | 3.11 |
| 42 | $\begin{gathered} 92102 \\ 1 \\ \hline \end{gathered}$ | 180927.53 | 29-46.47 | 31-12.00 | 14.65 | 2.7 | 1.97 |
| 43 | $\begin{gathered} 92102 \\ 2 \\ \hline \end{gathered}$ | 082858.70 | 29-44.83 | 31-6.53 | 21.90 | 3.4 | 3.42 |
| 44 | $\begin{gathered} 92102 \\ 2 \\ \hline \end{gathered}$ | 173857.30 | 29-40.62 | 31-5.68 | 22.88 | 3.9 | 4.59 |
| 45 | $\begin{gathered} 92102 \\ 3 \\ \hline \end{gathered}$ | 02405.43 | 29-44.21 | 31-5.46 | 22.85 | 2.6 | 2.17 |
| 46 | $\begin{gathered} 92102 \\ 3 \end{gathered}$ | 151210.08 | 29-41.39 | 31-10.00 | 22.40 | 3.8 | 3.29 |
| 47 | $\begin{gathered} 92102 \\ 3 \\ \hline \end{gathered}$ | 16024.12 | 29-44.78 | 31-7.38 | 21.70 | 2.4 | 1.7 |
| 48 | $\begin{gathered} 92102 \\ 5 \\ \hline \end{gathered}$ | 09054.64 | 29-40.09 | 31-10.71 | 22.05 | 3.1 | 2.8 |
| 49 | $\begin{gathered} 92102 \\ 5 \\ \hline \end{gathered}$ | 122615.06 | 29-39.93 | 31-5.95 | 24.12 | 3.1 | 2.72 |
| 50 | $\begin{gathered} 92102 \\ 5 \\ \hline \end{gathered}$ | 162105.28 | 29-38.35 | 31-6.70 | 22.92 | 2.9 | 2.31 |
| 51 | $\begin{gathered} 92102 \\ 5 \\ \hline \end{gathered}$ | 194534.56 | 29-40.97 | 31-8.52 | 23.78 | 2.3 | 3.16 |


| $\#$ | Date <br> M M D | Origin Time <br> H m s |  | Lat $^{\circ} \mathrm{N}$ | Lon $^{\circ} \mathrm{E}$ | Depth(Km) | MD <br> (HLW) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 52 | 92102 <br> 6 | 064523.96 | $29-52.40$ | $31-6.49$ | 27.45 | 3.4 | 3.27 |
| 53 | 92102 <br> 6 | 084352.01 | $29-40.55$ | $31-5.75$ | 28.25 | 2.8 | 2.41 |
| 54 | 92102 <br> 8 | 062054.90 | $29-37.30$ | $31-3.63$ | 24.63 | 2.9 | 2.51 |
| 55 | 92102 <br> 8 | 182556.28 | $29-50.64$ | $31-16.07$ | 19.46 | 2.8 | 2.45 |
| 56 | 92103 <br> 0 | 140811.19 | $29-40.70$ | $31-5.09$ | 25.71 | 3.0 | 2.74 |

Teleseismic body wave inversion of the mainshock (Hussein, 1999) suggest normal faulting mechanism with a small strike slip component on a plane striking E-W to WNWESE and dipping to the east. ( $\mathbf{F i g} \mathbf{( 3 )})$

The main objective of this study is to calculate the source parameters of the Cairo earthquake aftershocks recorded by the KEG Broad Band station during three weeks after the mainshock. In addition to develop scaling laws between spectral parameters (Seismic moment, Source radius and Stress drop) and time domain parameters (Coda length) and ML


Fig(3) : Fault plane solution of the mainshock

## 2-Data:

The 55 Dahshour aftershocks recorded during the two weeks after the occurrence of the mainshock of Oct 12,1992 earthquake were selected for the analysis. Event data are given in Table (1). The local magnitude (ML) of these events varied from 1.7 to 4.7. All of these earthquakes are of crustal origin. Seismic moment, source dimensions and radiated seismic energy were estimated from the digital records of KEG Broad Band station. KEG station is a part of the MEDNET project (Boschi et al, 1988). The seismic records were electronically digitized at a rate of 20 samples per second by STS-1 VBB velocity type sensor. For frequencies between 0.003 and 7 HZ the velocity response is flat with a full dynamic range of 140 dB .

## 3- Method of analysis:

In this work a time window that started shortly before the $\mathbf{L g}$ arrival, depending on the size of earthquake was obtained from the vertical component. The time window was nearly 10 sec . long. The digital data within the time window were corrected for the instrumental response, Fourier transformed to obtain the amplitude spectra and then integrated to obtain the displacement spectra. Typical spectrum examples are shown in Fig (4).
The spectrum was corrected for the attenuation, multiplying it by the transfer function $\mathbf{e}^{-\gamma r}$ where $\mathbf{r}$ is the distance from the source to the receiver and $\gamma$ is the coefficient of anelastic attenuation which is related to quality factor $\mathbf{Q}$ (Nuttli, 1986) by :
Where $\mathbf{f}$ is the wave frequency and $\mathbf{U}$ is the Lg wave group velocity. Dessoky et al, 1999 obtain a value of $\mathbf{0 . 0 0 1 4 9 5} \mathbf{~ k m}^{-1}$ for $\mathbf{1 ~ H z ~} \mathbf{L g}$ in Dahshour region.
From the corrected spectrum, the low frequency spectral level and the corner frequency were estimated. The low frequency level ( $\mathbf{\Omega 0}$ ) was estimated visually by fitting a straight line at the

$$
\begin{equation*}
\gamma=\frac{\pi \cdot f}{U \cdot Q} \tag{1}
\end{equation*}
$$

low frequency spectra. The corner frequency (fc) values were estimated by direct measurements of the low and high frequency trends of the spectra plotted in a double logarithmic scale.

The seismic moment (Mo) were derived for the 55 recorded events from the low spectral level ( $\Omega \mathbf{0}$ ) estimated using street et al., 1975 formula that was subsequently derived by means of theoretical modeling by Herrmann and Kyko, 1983

$$
\begin{array}{lll}
M o=4 \Pi \rho \beta^{3} R o(R / R o) & \Omega o & R<R o  \tag{2}\\
M o=4 \Pi \rho \beta^{3} R o(R / R o)^{1 / 2} \Omega o & R<R o
\end{array}
$$

Where $\rho$ is the density of the medium, $\beta$ is the shear wave velocity, $\mathbf{R}$ is the epicentral distance and Ro is a reference distance. The reference distance Ro was determined empirically by comparing values of seismic moment given by the above relation with those obtained by amplitude equalization of long period surface wave (e.g. from Hermann, 1974).

For a circular fault the source radius ro can be calculated from the corner frequency, with Brune's, (1970) relation:-

$$
\begin{equation*}
r_{o}=\frac{2.34 \beta}{2 \Pi f_{c}} \tag{3}
\end{equation*}
$$

Typical source radius values ranges from 0.26 to $0.65 \mathbf{k m}$.
The stress drop $\boldsymbol{\Delta} \boldsymbol{\delta}$ is given by the following relation (Keilis-Borok, 1959; Brune,1970).
The estimated stress drop varied from 0.12 to 120 bars. In this work radiated energy was also calculated following Boatwright (1980). The following equation was used to calculate the

$$
\begin{equation*}
\Delta \delta=\frac{0.44 M o}{r_{o}^{3}} \tag{4}
\end{equation*}
$$

radiated seismic energy in the body wave arrivals.

$$
\begin{equation*}
E s=\left(\frac{R}{F R_{\theta \phi}}\right)^{2} \cdot \frac{\rho(r) \beta(r)}{e(\theta, \phi)} I \tag{5}
\end{equation*}
$$



Fig (4): FFT spectrum of some selected events

Where $\mathbf{R}$ is the hypocentral distance, $\mathbf{F}$ is the free surface correction, $\mathbf{R}_{\boldsymbol{\theta}, \boldsymbol{\varphi}}$ is the radiation pattern coefficient, $\rho(\mathbf{r}), \beta(\mathbf{r})$ are the density and the shear wave velocity at the receiver respectively, $\mathbf{e}(\boldsymbol{\theta}, \boldsymbol{\varphi})$ is the fractional Energy flux and $\mathbf{I}$ is the integral of the square of the ground velocity and it is expressed as follows:

$$
\begin{equation*}
I=\int_{0}^{\infty} \breve{U}^{o}(r, t) d t=\frac{1}{\Pi} \int_{0}^{\infty}\left|U^{o}\right|^{2} d \omega \tag{6}
\end{equation*}
$$

Where $U(r, w)$ is the velocity spectrum.
The fractional energy flux relates the shear wave energy flux at a particular take off angle with the total radiated seismic energy.
The horizontal components for the selected aftershocks were rotated into their radial and transverse components before calculation in order to get reliable results. The Integral of the square of the ground velocities were taken from the KEG record after doing the appropriate analysis and squaring and take the appropriate window. The parameters calculated using the above formulas are listed in table (2)

## Results:

### 1.1 Seismic moment coda duration and local magnitude

The seismic moments of the events under study were estimated using equation (2). Constant values corresponding to Dahshour region in equation (2) were selected as follows: $\rho=\mathbf{2 . 7} \mathbf{~ g m} / \mathbf{c m}^{3}, \beta=\mathbf{3 . 5} \mathbf{~ k m} / \mathbf{s e c}$ and $\mathbf{R o}=\mathbf{1 0 0} \mathbf{~ k m}$. The seismic moments estimated was found to range from $2.26 \times 10^{22}$ to $\mathbf{2 . 8 \times 1 0 ^ { 1 9 }}$ dyne.cm. Table(2) show the resulted seismic moment as given in this study.

Mathematical regression between the reported seismic moments and the corresponding coda duration has been also done. The Coda duration used in this study were given from the available analog seismographic stations installed in the time of earthquake. It has been taken from the $\mathbf{P}$ arrival to the point in the coda where the seismic amplitude is nearly twice the background noise amplitude. The Linear regression fitting of the data as shown in $\mathbf{F i g}(\mathbf{5})$ indicates the following relation:

$$
\begin{equation*}
\log (M o)=(2.42 \pm 0.72) \log (D)+(16.21 \pm 1.32) \tag{7}
\end{equation*}
$$

The seismic moment - local magnitude relation is shown in $\mathbf{F i g}(\mathbf{6})$. The least square fit implies the following equation:

$$
\begin{equation*}
\log (M 0)=(0.96 \pm 0.2) M L+(17.89 \pm 0.56) \quad(1.7<M L<4.7) \tag{8}
\end{equation*}
$$

This relation is almost similar to that found in Mammoth lakes, California (Archuleta et al., 1982) where

$$
\begin{equation*}
\log (\mathrm{Mo})=(1.05 \pm 0.08) \mathrm{ML}+(17.76 \pm 0.33) \quad(0.5<\mathrm{ML}<6.5) \tag{9}
\end{equation*}
$$

Baukun and Lindah (1977) obtained the following relation for earthquake
located near Oroville,California

$$
\begin{equation*}
\log (\mathrm{Mo})=(1.21 \pm 0.03) \mathrm{ML}+(17.02 \pm 0.07) \quad(0<\mathrm{ML}<6) \tag{10}
\end{equation*}
$$

Which is also similar to equation (8)


Fig(5): Seismic moment (Mo) - Coda duration relation of Dashshour earthquake sequence


Fig(6): Seismic moment - Local magnitude relation

Table(2): Seismic moment, Stress drop, Source radius of the events under study.

| Event \# | Duration (sec) | ML | Mo (dyne.cm) | Stress drop (bar) | r0 (km) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1040 | 5.96 | $1.370604 \mathrm{E}+24$ | 270.3445 | 1.30414 |
| 2 |  | 2.52 | $1.942783 \mathrm{E}+20$ | 2.452504 | 0.326035 |
| 3 |  | 2.31 | $2.267175 \mathrm{E}+20$ | 1.917319 | 0.3726115 |
| 4 |  | 2.81 | $2.836813 \mathrm{E}+20$ | 3.581097 | 0.326035 |
| 5 |  | 1.84 | $5.468023 \mathrm{E}+19$ | 0.6902648 | 0.326035 |
| 6 |  | 2.34 | $7.922314 \mathrm{E}+19$ | 0.1250108 | 0.65207 |
| 7 | 279 | 4.7 | $2.267175 \mathrm{E}+22$ | 120.7408 | 0.4347134 |
| 8 |  | 2.26 | 8.386375E+19 | 0.2584638 | 0.4347134 |
| 9 |  | 2.37 | $1.225617 \mathrm{E}+20$ | 0.6527153 | 0.4347134 |
| 10 |  | 2.24 | $1.28611 \mathrm{E}+20$ | 1.183562 | 0.3622611 |
| 11 |  | 2.19 | $1.520192 \mathrm{E}+20$ | 2.221526 | 0.3105096 |
| 12 | 169 | 4.15 | $7.825914 \mathrm{E}+21$ | 98.79171 | 0.326035 |
| 13 | 57 | 2.45 | $1.021348 \mathrm{E}+20$ | 1.289315 | 0.326035 |
| 14 | 65 | 2.69 | $7.1504 \mathrm{E}+20$ | 9.026424 | 0.326035 |
| 15 |  | 2.13 | 8.689964E+19 | 0.4627932 | 0.4347134 |
| 16 | 161 | 3.67 | $2.028367 \mathrm{E}+21$ | 17.15362 | 0.3726115 |
| 17 | 92 | 3.16 | $7.671786 \mathrm{E}+20$ | 4.08569 | 0.4347134 |
| 18 | 37 | 2.22 | $6.70293 \mathrm{E}+19$ | 0.8461553 | 0.326035 |
| 19 | 56 | 2.77 | $3.1557 \mathrm{E}+20$ | 3.983649 | 0.326035 |
| 20 |  | 2.76 | $4.717935 \mathrm{E}+20$ | 5.955762 | 0.326035 |
| 21 | 237 | 4.17 | $5.429151 \mathrm{E}+21$ | 68.53578 | 0.326035 |
| 22 |  | 1.94 | $5.667937 \mathrm{E}+19$ | 0.7155013 | 0.326035 |
| 23 | 34 | 2.95 | $3.666106 \mathrm{E}+20$ | 1.952423 | 0.4347134 |
| 24 |  | 3.22 | $4.157197 \mathrm{E}+20$ | 2.213959 | 0.4347134 |
| 25 |  | 2.4 | $4.071058 \mathrm{E}+20$ | 3.442838 | 0.3726115 |
| 26 | 69 | 2.92 | $4.769604 \mathrm{E}+20$ | 2.540103 | 0.4347134 |
| 27 | 45 | 2.29 | $6.387174 \mathrm{E}+19$ | 0.3401557 | 0.4347134 |
| 28 | 35 | 1.96 | $6.550127 \mathrm{E}+19$ | 0.5539353 | 0.3726115 |
| 29 |  | 1.99 | $3.571662 \mathrm{E}+19$ | 0.8806145 | 0.260828 |
| 30 | 108 | 2.91 | 5.07458E+20 | 6.405979 | 0.326035 |
| 31 | 62 | 3.08 | $7.187676 \mathrm{E}+20$ | 3.827873 | 0.4347134 |
| 32 |  | 2.4 | $2.237957 \mathrm{E}+20$ | 1.191848 | 0.4347134 |
| 33 | 35 | 2.03 | $6.845436 \mathrm{E}+19$ | 0.5789092 | 0.3726115 |
| 34 | 78 | 2.86 | $4.614945 \mathrm{E}+20$ | 5.825751 | 0.326035 |
| 35 | 63 | 2.61 | $3.037181 \mathrm{E}+20$ | 3.834035 | 0.326035 |
| 36 | 39 | 2.23 | $9.024836 \mathrm{E}+19$ | 0.4806272 | 0.4347134 |
| 37 | 85 | 2.99 | $7.510935 \mathrm{E}+20$ | 9.481552 | 0.326035 |
| 38 | 79 | 3.17 | 6.659202E+20 | 5.631596 | 0.3726115 |
| 39 |  | 1.65 | $2.856025 \mathrm{E}+19$ | 0.360535 | 0.326035 |
| 40 | 30 | 1.98 | 5.832978E+19 | 0.7363355 | 0.326035 |
| 41 | 87 | 3.11 | $9.421127 \mathrm{E}+20$ | 5.017321 | 0.4347134 |
| 42 |  | 1.97 | $6.235795 \mathrm{E}+19$ | 0.5273526 | 0.3726115 |
| 43 | 94 | 3.42 | $1.637872 \mathrm{E}+21$ | 8.72266 | 0.4347134 |
| 44 |  | 4.59 | $2.522325 \mathrm{E}+22$ | 118.4098 | 0.4075438 |
| 45 | 34 | 2.17 | $1.227609 \mathrm{E}+20$ | 0.6537762 | 0.4347134 |
| 46 |  | 3.29 | $1.490997 \mathrm{E}+21$ | 7.940462 | 0.4347134 |
| 47 |  | 1.7 | $3.499786 \mathrm{E}+19$ | 0.2959721 | 0.3726115 |
| 48 | 55 | 2.8 | $4.527036 \mathrm{E}+20$ | 2.410921 | 0.4347134 |
| 49 | 68 | 2.72 | $5.052129 \mathrm{E}+20$ | 2.690565 | 0.4347134 |
| 50 | 38 | 2.31 | $1.011922 \mathrm{E}+20$ | 0.8557686 | 0.3726115 |
| 51 |  | 3.16 | $7.076904 \mathrm{E}+20$ | 3.76888 | 0.4347134 |


| Event \# | Duration (sec) | ML | Mo (dyne.cm) | Stress drop (bar) | r0 (km) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 52 | 99 | 3.27 | $1.602396 \mathrm{E}+21$ | 8.533729 | 0.4347134 |
| 53 | 34 | 2.41 | $1.00893 \mathrm{E}+20$ | 1.273639 | $\mathbf{0 . 3 2 6 0 3 5}$ |
| 54 | 59 | 2.51 | $2.729787 \mathrm{E}+20$ | 0.4307489 | 0.65207 |
| 55 | 50 | 2.45 | $1.03903 \mathrm{E}+20$ | $\mathbf{0 . 5 5 3 3 4 6 4}$ | 0.4347134 |
| 56 |  | 2.74 | $\mathbf{3 . 8 3 4 0 3 6 E}+20$ | $\mathbf{2 . 0 4 1 8 5 6}$ | 0.4347134 |

### 1.2 Seismic moment,Source radius and Stress drop relationships:

The scaling relation between the seismic moment and source radius is shown in $\mathbf{F i g}(7)$.
Most of earthquakes in this study have stress drops between 0.1 and 10 bars. Source radii ranges from 0.26 to 0.65 km . Events of seismic moment less than $10^{21}$ dyne.cm have nearly constant source radii that corresponds to decreasing of stress drop with seismic moment decrease the thing that has been observed in several recent strudies (e.g. Kim et al, 1989 and Valdes and Meger,1996,Dysart et al.,1988). Asperities and barriers are the physical basis of this phenomena where the slip varies more than one order of magnitude while the fault length remains constant.
For Events of seismic moment greater than $10^{21}$ dyne.cm, although, there is not enough data that lie in this range, it seems that there is increase of source radius with increase seismic moment while the stress drop remain constant.


Fig (7): Seismic moment - Stress drop relationship

## Radiated Energy relationships

The radiated energies of both the SH and SV velocity time series from the window previously used in the Fourier analysis was obtained from Equation (5)
In this analysis we used $R_{\theta, \varphi}=\mathbf{0 . 6}, \beta=5.5 \mathrm{Km} / \mathbf{s e c}, \rho=\mathbf{2 . 7} \mathbf{g m} / \mathrm{cm}^{3}, \mathbf{f}=\mathbf{2}$ and $\mathbf{e}(\boldsymbol{\theta}, \varphi)=1 / 2 \Pi$ (based on randall,1973).
The resulting estimates of the radiated seismic energy for both radiated and transverse components are compiled in table
The mathematical fitting between the local magnitude (ML) and the average radiated energy estimated in this study is shown in Fig (8) the corresponding empirical relation in given by:

$$
\begin{equation*}
\log (E)=(1.752 \pm 0.03) M L+(12.86 \pm 0.09) \tag{11}
\end{equation*}
$$

Fig(10) Shows the Seismic moment values of the given earthquakes plotted versus their corresponding average radiated energy, the derived equation is as follows:

$$
\log (E s)=(1.74 \pm 0.059) \log (M o)-(18.07 \pm 1.2)
$$

(12)

Table(3): Radiated energy values of the events under study.

| \# | ML | I (rad) | I (trans) | Es(rad) erg | Es(trans) erg | E(average) erg |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 5.96 | 1.5 | 3 | $8.405 \mathrm{E}+23$ | $1.681 \mathrm{E}+24$ | 1.26075E+24 |
| 2 | 2.52 | 0.0000008 | 0.0000009 | 2.42406E+17 | $2.727067 \mathrm{E}+17$ | $2.575563 \mathrm{E}+17$ |
| 3 | 2.31 | 4E-8 | 0.0000004 | $1.60083 \mathrm{E}+16$ | $1.60083 \mathrm{E}+17$ | 8.804565E+16 |
| 4 | 2.81 | 0.000001 | 0.0000015 | $5.950209 \mathrm{E}+17$ | 8.925313E+17 | $7.437761 \mathrm{E}+17$ |
| 5 | 1.84 | 5.5E-8 | 2E-8 | $1.483905 \mathrm{E}+16$ | $5.396017 \mathrm{E}+15$ | $1.011753 \mathrm{E}+16$ |
| 6 | 2.34 | 0.0000002 | 0.0000015 | $7.981066 \mathrm{E}+16$ | 5.9858E+17 | $3.391953 \mathrm{E}+17$ |
| 7 | 4.7 | 0.0025 | 0.00215 | $1.000519 \mathrm{E}+21$ | 8.604462E+20 | 9.304826E+20 |
| 8 | 2.26 | 1.4E-7 | 1.1E-7 | $4.868686 \mathrm{E}+16$ | $3.825396 \mathrm{E}+16$ | $4.347041 \mathrm{E}+16$ |
| 9 | 2.37 | 0.0000003 | 0.0000003 | $9.954025 \mathrm{E}+16$ | $9.954025 \mathrm{E}+16$ | 9.954025E+16 |
| 10 | 2.24 | 1.6E-7 | 0.0000002 | $5.790413 \mathrm{E}+16$ | $7.238017 \mathrm{E}+16$ | 6.514215E+16 |
| 11 | 2.19 | 1.75E-7 | 2.2E-7 | $5.093681 \mathrm{E}+16$ | $6.403485 \mathrm{E}+16$ | $5.748583 \mathrm{E}+16$ |
| 12 | 4.15 | 0.0003 | 0.00029 | $1.540563 \mathrm{E}+20$ | $1.48921 \mathrm{E}+20$ | $1.514887 \mathrm{E}+20$ |
| 13 | 2.45 | 0.0000003 | 4.25E-7 | $9.954025 \mathrm{E}+16$ | $1.410153 \mathrm{E}+17$ | 1.202778E+17 |
| 14 | 2.69 | 0.0000015 | 0.0000012 | $3.906013 \mathrm{E}+17$ | 3.12481E+17 | $3.515411 \mathrm{E}+17$ |
| 15 | 2.13 | 8.5E-8 | 8E-8 | $3.151297 \mathrm{E}+16$ | $2.965926 \mathrm{E}+16$ | 3.058612E+16 |
| 16 | 3.67 | 0.00005 | 0.0000475 | $1.638037 \mathrm{E}+19$ | $1.556136 \mathrm{E}+19$ | $1.597086 \mathrm{E}+19$ |
| 17 | 3.16 | 0.0000075 | 0.0000055 | $2.2201 \mathrm{E}+18$ | $1.628073 \mathrm{E}+18$ | $1.924087 \mathrm{E}+18$ |
| 18 | 2.22 | 1.3E-7 | 2.5E-7 | $5.06844 \mathrm{E}+16$ | $9.747 \mathrm{E}+16$ | $7.40772 \mathrm{E}+16$ |
| 19 | 2.77 | 0.0000016 | $1.25 \mathrm{E}-6$ | $5.59872 \mathrm{E}+17$ | $4.374 \mathrm{E}+17$ | $4.98636 \mathrm{E}+17$ |
| 20 | 2.76 | 0.0000015 | $1.65 \mathrm{E}-6$ | $6.444051 \mathrm{E}+17$ | $7.088455 \mathrm{E}+17$ | 6.766253E+17 |
| 21 | 4.17 | 0.0004 | 0.00025 | $2.20323 \mathrm{E}+20$ | $1.377019 \mathrm{E}+20$ | $1.790125 \mathrm{E}+20$ |
| 22 | 1.94 | 4E-8 | 5.5E-8 | $1.60083 \mathrm{E}+16$ | $2.201142 \mathrm{E}+16$ | $1.900986 \mathrm{E}+16$ |
| 23 | 2.95 | 0.0000013 | 1.25E-6 | 5.948377E+17 | 5.719594E+17 | $5.833985 \mathrm{E}+17$ |
| 24 | 3.22 | 0.00001 | 0.0000085 | $3.424008 \mathrm{E}+18$ | $2.910407 \mathrm{E}+18$ | $3.167208 \mathrm{E}+18$ |
| 25 | 2.4 | 0.0000004 | 0.0000005 | $1.318803 \mathrm{E}+17$ | $1.648504 \mathrm{E}+17$ | $1.483654 \mathrm{E}+17$ |
| 26 | 2.92 | 0.0000025 | 0.0000026 | $1.095052 \mathrm{E}+18$ | $1.138854 \mathrm{E}+18$ | $1.116953 \mathrm{E}+18$ |
| 27 | 2.29 | 1.8E-7 | 1.9E-7 | 6.435375E+16 | 6.792896E+16 | 6.614135E+16 |
| 28 | 1.96 | $4.5 \mathrm{E}-8$ | 4.5E-8 | $1.683375 \mathrm{E}+16$ | $1.683375 \mathrm{E}+16$ | $1.683375 \mathrm{E}+16$ |
| 29 | 1.99 | 3.9E-8 | 4E-8 | $1.703572 \mathrm{E}+16$ | $1.747253 \mathrm{E}+16$ | 1.725412E+16 |
| 30 | 2.91 | 0.0000025 | 0.0000019 | $1.222408 \mathrm{E}+18$ | $9.290303 \mathrm{E}+17$ | $1.075719 \mathrm{E}+18$ |
| 31 | 3.08 | 0.0000037 | 0.000004 | $1.634117 \mathrm{E}+18$ | $1.766614 \mathrm{E}+18$ | $1.700366 \mathrm{E}+18$ |
| 32 | 2.4 | 0.0000004 | 4.5E-7 | $1.564083 \mathrm{E}+17$ | $1.759594 \mathrm{E}+17$ | $1.661838 \mathrm{E}+17$ |
| 33 | 2.03 | 5.5E-8 | 6.5E-8 | $2.226624 \mathrm{E}+16$ | $2.631465 \mathrm{E}+16$ | $2.429045 \mathrm{E}+16$ |
| 34 | 2.86 | 0.000002 | 0.0000025 | $8.260267 \mathrm{E}+17$ | $1.032533 \mathrm{E}+18$ | 9.292799E+17 |
| 35 | 2.61 | 8.5E-7 | 0.0000009 | $2.775788 \mathrm{E}+17$ | $2.93907 \mathrm{E}+17$ | $2.857429 \mathrm{E}+17$ |
| 36 | 2.23 | 0.0000001 | 1.1E-7 | $3.9675 \mathrm{E}+16$ | $4.36425 \mathrm{E}+16$ | $4.165875 \mathrm{E}+16$ |
| 37 | 2.99 | 0.0000035 | 0.000005 | $1.671393 \mathrm{E}+18$ | $2.387704 \mathrm{E}+18$ | $2.029549 \mathrm{E}+18$ |
| 38 | 3.17 | 3.25E-6 | 2.75E-6 | $1.252333 \mathrm{E}+18$ | $1.059667 \mathrm{E}+18$ | $1.156 \mathrm{E}+18$ |
| 39 | 1.65 | $1.25 \mathrm{E}-8$ | 1.5E-8 | $7.526042 \mathrm{E}+15$ | $9.03125 \mathrm{E}+15$ | $8.278646 \mathrm{E}+15$ |
| 40 | 1.98 | 4E-8 | 4.5E-8 | $1.68507 \mathrm{E}+16$ | $1.895704 \mathrm{E}+16$ | $1.790387 \mathrm{E}+16$ |
| 41 | 3.11 | 0.000005 | 0.0000068 | $2.142037 \mathrm{E}+18$ | $2.913171 \mathrm{E}+18$ | $2.527604 \mathrm{E}+18$ |
| 42 | 1.97 | 5.5E-8 | 1.5E-7 | $1.883204 \mathrm{E}+16$ | $5.136013 \mathrm{E}+16$ | $3.509608 \mathrm{E}+16$ |
| 43 | 3.42 | 0.000013 | 0.000015 | $7.23113 \mathrm{E}+18$ | 8.343612E+18 | $7.787371 \mathrm{E}+18$ |
| 44 | 4.59 | 0.0017 | 0.0022 | $8.22579 \mathrm{E}+20$ | $1.064514 \mathrm{E}+21$ | $9.435465 \mathrm{E}+20$ |
| 45 | 2.17 | 0.0000001 | 9E-8 | $4.6128 \mathrm{E}+16$ | $4.15152 \mathrm{E}+16$ | $4.38216 \mathrm{E}+16$ |
| 46 | 3.29 | 0.000011 | 0.000011 | $5.183786 \mathrm{E}+18$ | 5.183786E+18 | $5.183786 \mathrm{E}+18$ |


| 47 | 1.7 | 1.5E-8 | 1.5E-8 | 6.319012E+15 | 6.319012E+15 | 6.319012E+15 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | ML | I (rad) | I (trans) | Es(rad) erg | Es(trans) erg | E(average) erg |
| 48 | 2.8 | 0.000002 | 0.0000018 | 7.981066E+17 | 7.182959E+17 | $7.582012 \mathrm{E}+17$ |
| 49 | 2.72 | 0.0000011 | 1.35E-6 | $5.336549 \mathrm{E}+17$ | $6.549402 \mathrm{E}+17$ | 5.942976E+17 |
| 50 | 2.31 | 1.4E-7 | 1.7E-7 | $6.809787 \mathrm{E}+16$ | 8.269028E+16 | $7.539408 \mathrm{E}+16$ |
| 51 | 3.16 | 0.0000046 | 0.0000057 | $1.976175 \mathrm{E}+18$ | $2.448739 \mathrm{E}+18$ | $2.212457 \mathrm{E}+18$ |
| 52 | 3.27 | 0.000018 | 0.000015 | $7.329016 \mathrm{E}+18$ | 6.107513E+18 | $6.718265 \mathrm{E}+18$ |
| 53 | 2.41 | 0.0000005 | 0.0000001 | $2.41935 \mathrm{E}+17$ | $4.8387 \mathrm{E}+16$ | $1.45161 \mathrm{E}+17$ |
| 54 | 2.51 | 2.75E-7 | 3.6E-7 | $1.529662 \mathrm{E}+17$ | $2.002467 \mathrm{E}+17$ | $1.766064 \mathrm{E}+17$ |
| 55 | 2.45 | 1.6E-7 | 1.3E-7 | 3.93132E+16 | $\mathbf{3 . 1 9 4 1 9 7 E}+16$ | $3.562759 \mathrm{E}+16$ |
| 56 | 2.74 | 5.5E-7 | 0.0000006 | $2.724521 \mathrm{E}+17$ | 2.972205E+17 | $2.848363 \mathrm{E}+17$ |



Fig(9): Average Energy - ML Relationship.


Fig(10) Radiated energy - Seismic moment relationship

## Conclusions:

Seismic moment Mo, logarithm of the coda duration and the local magnitude empirical relations were derived for the aftershocks of 1992 Cairo earthquakes source area, providing a simple and straightforward way to qualify the source strength M0 through such relationships. The obtained relations are similar to those reported in other sites indicating that such relations may not change in different tectonic provinces.
The source estimates for the earthquakes with the seismic moment less than $10^{21}$ N.m. remain nearly constant. This tendency should be attributed to source effect. Similar situations have been observed in many regions where the stress drop decrease with decreasing seismic moment in this range.
The energy release was also calculated in this study. The Log Energy versus Log local magnitude and Log energy versus log moment was derived. The energy released versus magnitude is nearly the same as the expected theoretical value of Gutenberg and Richter, 1956 (Log Es=1.92 ML).

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